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MULTICOMPONENT OHMIC CONTACTS TO GaAs

The paper contains the results of the study of semiconductor wafer preprocessing, application and heat treatment modes of Ag-GE-In/n-n Ga As contacts impact on specific transient resistance.

Key words: gallium-arsenide, ternary alloy, vacuum deposition, heat treatment, specific resistance, ohmic contact.

Introduction

One of the most important technological operations, used for fabrication of semiconductor devices and integrated micro circuits, based on gallium –arsenide is the formation of ohmic contacts (OC) [1, 2]. For the creation of OC binary or more complex alloys on the base of copper, silver, gold, palladium with admixture of metals (cadmium, magnesium aluminium, indium and others [2 - 5]), easily oxidizing, are used.

Erosion strength of this group of alloys is based on protective action of oxide films, preventing evaporation but not preventing contact conductivity. The value of contact resistance of ohmic contact is determined, to a considerable extent, by the technology of its fabrication [3 - 11].

The aim of the given research is study and determination of the impact of semiconductor wafer preprocessing, modes of deposition and heat treatment of Ag-Ge-In/n-n⁺GaAs contacts on specific transient resistance.

Experimental study

For investigation $n - n^+GaAs(111)B$ epitaxial monocrystal with epitaxial layer thickness of $d_{e.l.}=2$ m μ , carriers concentration in epilaxial layer $n_{e.l.}=2 \cdot 10^{16}$ cm⁻³, carriers concentration in the substrate $n_{sub}=10^{18}$ cm⁻³ and mobility μ >5000 cm²/(V·c) was used.

For OC creation to gallium-arcenide ternary alloy Ag-Ge-In (75%-20%-5% by weight, correspondingly) is chosen, where Ag-basic material, Ge-dopping admixture and In improves wettability. Silver alloys of the similar type are rather stable to corrosion, keeping low contact resistance [3 – 5, 8 – 12]. Silver under the action of electric charges oxidizes but silver oxides have good electric conductivity and easily dissociate (dissociation temperature~ 573 K). As a result, oxidization exercises minor impact on the stability of conduct resistance of silver contacts.

For fabrication of ohmic contacts it is necessary to get near the surface of semiconductor the concentration of admixtures 10^{18} cm⁻³. There exists various methods [2] of increasing charge carriers concentration in the surface layers. Doping of the surface with metal occurs in the process of surface processing of the semiconductor in the solutions [13 - 16], containing admixtures of various metals.

Chemical smoothing of semiconductor substrate is performed to remove fins and decrease surface roughness. Characteristic feature of *GaAs* compound is different dissolution rate of the semiconductor on the plane (11) with the facets A and B with different character of chemical bonds of substrate atoms. Applying the same etching agent side (III) B is polished (smooth, clear), side (III) A- dim with developed mosaic structure [14].

Comparative analysis of the known polishing etching agents showed that among etching agents, used for chemical smoothing [13 - 16] of *GaAs*, etching in sulfurous agent provides more qualitative surface.

In the process of chemical treatment of GaAs plates in sulfurous etching agent $H_2SO_4:H_2O_2:H_2O$ (3:1:1) additional aging of the plate during $(1...1,3)\cdot10^3$ seconds in dihydroxy-syccnic acid HOOC-CH(OH)-CH(OH)-COOH with further washing in hot, cold distilled and deionized water and in methyl alcohol is recommended. It is established that aging in dihydroxy-succinic acid during $(1...1,3)\cdot10^3$ sec after chemical polishing in the mixture $3H_2SO_4-1H_2O_2-1H_2O$ decreases the value of specific contact resistance to $5\cdot10^{-5}$ ohm cm².

Impact of preliminary annealing of gallium-arsenide plates on specific contact resistance of the contact Ag-Ge-In/n-n⁺GaAs at temperatures of 673.... 873 K during 30...150 sec is investigated (Table 1).

Table 1

Temperature of preliminary	Specific contract resistance of contacts ρ_c , Ohm·cm ²				
annealing of GaAs -substrate,	Batches of GaAsplates				
К	Nº1	N <u>⁰</u> 2	Nº3	<u>№</u> 4	N⁰5
673	9·10 ⁻²	$7 \cdot 10^{-2}$	8·10 ⁻²	5·10 ⁻²	$4 \cdot 10^{-2}$
698	8,6·10 ⁻²	$7,50.10^{-2}$	$5 \cdot 10^{-2}$	$7,5 \cdot 10^{-2}$	4,3.10-2
723	8·10 ⁻²	8·10 ⁻²	3.10-2	9·10 ⁻²	5·10 ⁻²
748	$7,15 \cdot 10^{-2}$	$1 \cdot 10^{-2}$	9·10 ⁻³	$2 \cdot 10^{-2}$	$2 \cdot 10^{-2}$
773	$6 \cdot 10^{-2}$	$5 \cdot 10^{-3}$	$4 \cdot 10^{-3}$	$3 \cdot 10^{-3}$	$7 \cdot 10^{-3}$
798	6·10 ⁻³	$2 \cdot 10^{-3}$	$1 \cdot 10^{-3}$	$1 \cdot 10^{-3}$	$2,5 \cdot 10^{-3}$
823	$7 \cdot 10^{-4}$	9·10 ⁻⁴	$5 \cdot 10^{-4}$	$3 \cdot 10^{-4}$	$7 \cdot 10^{-4}$
848	3.10-4	$3 \cdot 10^{-4}$	$1 \cdot 10^{-4}$	$1,5 \cdot 10^{-4}$	$1,2.10^{-4}$
873	8·10 ⁻⁵	$5 \cdot 10^{-5}$	8·10 ⁻⁵	9·10 ⁻⁵	$7 \cdot 10^{-5}$
Time of annealing, sec	30	60	90	120	150

Specific contact resistance ρ_c of Ag-Ge-In/n-n⁺GaAs contacts, substrate of which was annealed

It is established (Fig. 1) that preliminary temperature annealing of the substrate at 873 K during 60 sec in vacuum at residual pressure of $2 \cdot 10^{-6}$ Torr decreases the value of specific transient resistance of ohmic contacts to $\rho_c = (5...7) \cdot 10^{-5}$ Ohm·cm².

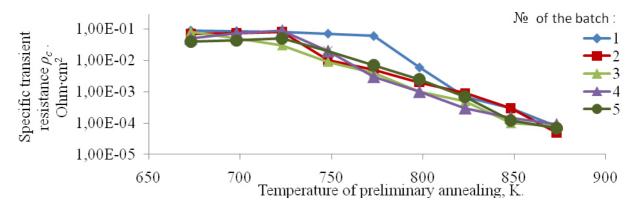


Fig. 1. Impact of preliminary annealing of the substrate on specific transient resistance of the contact Ag-Ge-In/n-n⁺GaAs

Thus, it is proved, that the quality of ohmic contact improves if GaAs substrate after chemical treatment in sulfurous etching agent, is kept in dihydroxy-succinic acid during $1.2 \cdot 10^3$ sec and additionally annealed in vacuum with the degree not less than $1.2 \cdot 10^{-6}$ Torr at the temperature of 873 K during 60 sec.

Application of contact material was performed by vacuum evaporation method at residual pressure of at least $1.2 \cdot 10^{-6}$ Torr. Measurements of contact resistance was carried out by compensation method [17, 18]. Calculation of specific transient resistance of OC was performed on the base of equivalent circuits method [17, 18].

Formation of the structure of ohmic contact by means of annealing was carried out in vacuum with the degree of not less than $(2...6) \cdot 10^{-6}$ Torr. Contact annealing to GaAs is necessary for introduction in the area of contact boundary the admixture or defects. Scientific Works of VNTU, 2017, № 3

The impact of the substrate temperature on specific transient resistance of the contact in the process of contact material application by the method of thermal evaporation, annealing temperature velocity increase, temperature and the time of annealing , contact cooling velocity is studied. For calculation of specific transient resistance value the formula [17] was used:

$$\rho_k = \frac{R_k b}{k \quad cth(ka)},\tag{1}$$

where R_c – complete resistance of the contact, P_c -specific transient resistance of the contact, a – width of the contact, b – length of the contact, ρ_{cc} -surface resistance of semiconductor. Values of k, corresponding to the values of R_c , are found from the graphic solution of the equation $y_1 = cka$, $y_2 = cth(ka)$, where $c = R_c \cdot b/(\rho_{cc} \cdot a)$.

Measurement limits of k numerical values are taken from the condition (17), that ρ_c/ρ_{sc} is less than one order (k=0,1÷10) in accordance with general requirements to the contacts. It is obvious, that in case, when the value of metal-semiconductor contact resistance $R_c > \rho_{sc}$, then specific contact resistance of the contact, reduced to the unit of the area, $\rho_c \text{ red} > \rho_{sc}$, the phenomenon of spreading currents, passing across the contact, is observed in near contact area. At optimal mode p_c of the contact is «pure» at $\rho_c \leq \rho_{sc}$. If $\rho_c > \rho_{sc}$ specific transient resistance consists only of transient resistance of spreading in near contact area.

Basic measurements error, in this case, expressed in % from rated value of measured resistance at the temperature of 293±2 K and relative humidity of the air 80%, did not exceed the following values : $a\pm 0.1\%$ within the limits of $10^{-3}-10^{-2}$ Ohm, b) $\pm 0.05\%$ within the limits of $10^{-2}-10^{-8}$ Ohm.

The choice of optimal values of heat treatment of contacts to *GaAs* with $n_{e.l.}=2\cdot10^{16}$ cm⁻³ .is determined by the necessity to create the layer with increased concentration of electrons due to doping with germanium. Contact annealing mode must provide minimal specific transient resistance of the contact and shallow occurrence of metal-semiconductor interface.

Contact material deposition was carried out on preheated substrate (Table 2).

Table 2

Impact of substrate temperature on specific transient resistance of the contacts $\rho_c Ag$ -Ge-In/n-n⁺GaAs

	Specific transient resistance, Ohm·cm ²			
Substrate temperature, K	№ of the batch			
	1	2	3	
423	$2 \cdot 10^{-2}$	$1,5.10^{-2}$	3.10-2	
453	6·10 ⁻⁵	$4 \cdot 10^{-5}$	7.10^{-5}	
483	8·10 ⁻⁴	5.10-4	$4 \cdot 10^{-4}$	
513	8·10 ⁻³	9·10 ⁻³	6·10 ⁻³	

By the results of research (Table 2) the best adhesion of contact material to gallium-arsenide was obtained at the temperature of the substrate 435 K, $\rho_c = (4...7) \cdot 10^{-5}$ Ohm cm².

The dependence of specific transient resistance of ohmic contacts ρ_c on the temperature and time of annealing in the range of temperatures 693... 943 K and time of annealing 60...300 sec. was studied (Fig. 2).

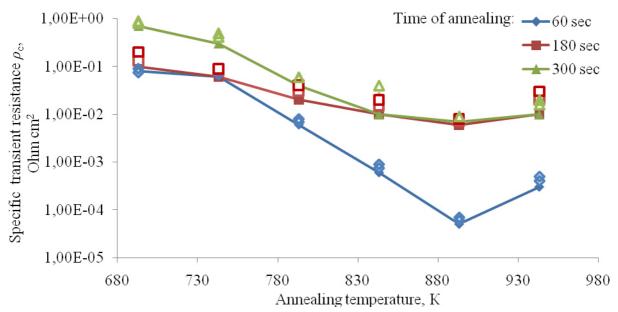


Fig. 2. Impact of the temperature and time of annealing on specific transient resistance ρ_c of Ag-Ge-In/n-n⁺GaAs contacts

It is established, that time and temperature of contact structure annealing greatly influence the quality of ohmic contact. The best results $\rho_c = (5...7) \cdot 10^{-5}$ Ohm cm² are obtained at the temperature of annealing 893 K and time of annealing 60 sec.

Linearity of VAC of the manufactured ohmic contacts was not violated in case of heating to the temperature of 453 K (Fig. 3).

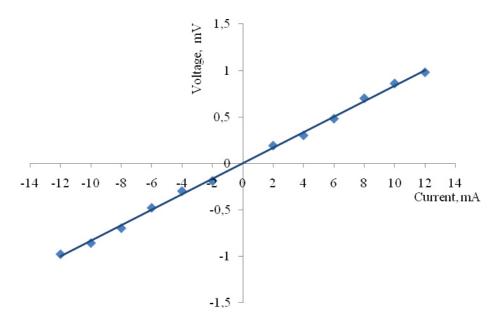


Fig. 3. Voltage-current characteristic of ohmic contact Ag-Ge-In/n-n⁺GaAs T_{an} =893 K, T_{an} =60 sec

The impact of the rate of annealing temperature increase in the range of 4.8....7.2 K\s and velocity of contact cooling in the range 465..475 K\s on the value of specific transient resistance of ohmic contacts ρ_c was studied (Fig. 4).

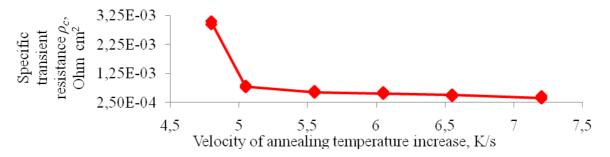


Fig..4. Dependence of specific transient resistance of ohmic contacts pc on the velocity of annealing temperature increase.

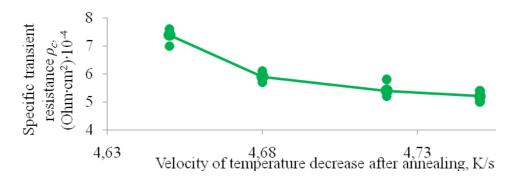


Fig. 5. Dependence of specific transient resistance of ohmic contacts pc on the velocity of contact cooling

It is established, that the increase of annealing temperature velocity from 5.55 K/s to 7.2 K/s leads to a slight decrease of specific transient resistance value (Fig. 4). Recommended velocity of annealing temperature increase 7.2 K/s.

Variation of contact cooling rate after annealing within the interval of 4.72, 4.75 K/s (Fig. 5) does not practically influence the value of specific transient resistance . Recommended velocity of contact cooling after annealing 4.75 K/s.

Conclusions

It is proved, that the additional aging in dihydroxy succinic acid after treatment in sulfuroms etching agent and preliminary annealing in vacuum of GaAs substrate at 873 K during 60 sec. decreases specific transient resistance of ohmic contact Ag-Ge-In/n- n^+GaAs .

Ohmic barrier junctions, based on ternary allow Ag-Ge-In (75% Ag, 20% Ge, 5% In) in GaAs c $n_{e.l.}=2\cdot10^{16}$ cm⁻³ provide rather low contact resistance $\rho_c = (5...7)\cdot10^{-5}$ Ohm·cm² and linearity of VAC in the process of contact material deposition on the substrate, heated to the temperature of 453 K and annealing of the obtained structure at 893 K during 60 sec. in vacuum at residual pressure of at least $1.2\cdot10^{-6}$ Torr, velocity of annealing temperature growth 7.2 K/s, and velocity of contact cooling after annealing 4.75 K/s.

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