

M. Baci, Dc. Sc. (Eng.), Ass. Prof.; I. Rusu, Dc. Sc. (Eng.), Ass. Prof.

INFLUENCE OF ELECTROLYTIC PLASMA NITRIDING ON PHASIC COMPOSITION OF 40Cr10 AND OLC 55 STEELS

The X-ray diffraction researches allowed the identification of the phases present in the structure of steels 40Cr10 and OLC 55, treated thermally and thermal-chemically in electrolytic plasma and the calculation of concentration of the structural phases identified.

Key words: electrolytic plasma, steels, nitration, X-ray diffraction.

1. Introduction

The analysis of the phasic composition of the steels 40Cr10 and OLC 55, treated thermally and thermal-chemically in electrolytic plasma allows the establishing of a correlation between the technological parameters of the processing methods and the physical-mechanical properties obtained in the end.

The experimental determinations were effectuated by X-ray diffraction, the analysis of diffraction diagrams allowing the identification of phases present in the structure of each sample and the calculation of the plane spacing d_{hkl} and the phase concentration.

2. Experimental procedure

The experimental researches were effectuated by cylindrical samples $\varnothing 15 \times 50$ mm, from the steels 40Cr10 and OLC 55, processed thermally by anodic heating in watery electrolytes according to the conditions presented in table 1.

Table 1

Technological parameters of thermal and thermal-chemical treatment in electrolytic plasma

No. crt.	Steel type	Sample	Thermal and thermal-chemical treatment applied	Technological parameters of thermal processing
1	40Cr10	3B	nitration + tempering + bluing	$T_{inc} = 650^{\circ}\text{C}$; $t_{inc} = 6$ min $T_{rev} = 350^{\circ}\text{C}$; $t_{rev} = 1$ h
2		3D	nitration + tempering	$T_{inc} = 700^{\circ}\text{C}$; $t_{inc} = 6$ min
3		3HH	nitration + tempering + bluing	$T_{inc} = 750^{\circ}\text{C}$; $t_{inc} = 6$ min $T_{rev} = 350^{\circ}\text{C}$; $t_{rev} = 1$ h
4		3A	nitration + tempering	$T_{inc} = 650^{\circ}\text{C}$; $t_{inc} = 6$ min $T_{aust} = 750^{\circ}\text{C}$
5	OLC 55	4V	nitration + tempering + bluing	$T_{inc} = 650^{\circ}\text{C}$; $t_{inc} = 6$ min $T_{rev} = 350^{\circ}\text{C}$; $t_{rev} = 1$ h
6		4DD	nitration + tempering	$T_{inc} = 700^{\circ}\text{C}$; $t_{inc} = 6$ min
7		4MM	nitration + tempering + bluing	$T_{inc} = 750^{\circ}\text{C}$; $t_{inc} = 6$ min $T_{rev} = 350^{\circ}\text{C}$; $t_{rev} = 1$ h
8		4Y	nitration + tempering	$T_{inc} = 650^{\circ}\text{C}$; $t_{inc} = 6$ min $T_{aust} = 750^{\circ}\text{C}$

The diffraction diagrams were obtained by the device DRON 2, using radiations MoK_{α} and FeK_{α} . The interval analysed is comprised between: $2\theta = 15^{\circ} \dots 40^{\circ}$

3. Experimental results

In figures 1...8 we present the diffraction diagrams obtained.

On the diffraction diagrams we identify the peaks of high intensity specific to phases and diffraction planes:

- austenite: (111); (200); (220); (311);
- martensite: (110); (200); (211);

- nitrides: Fe_3N

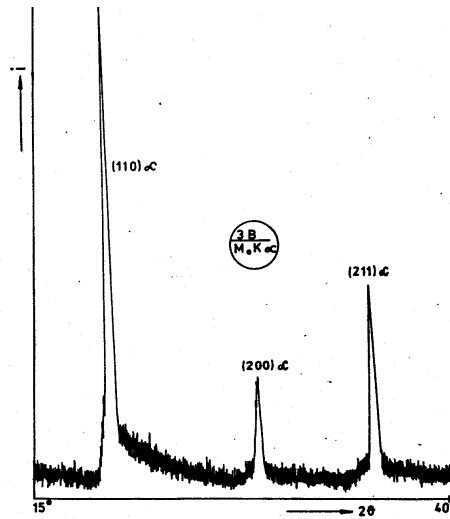


Fig. 1. Diffraction diagram of steel 40Cr10 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 3B

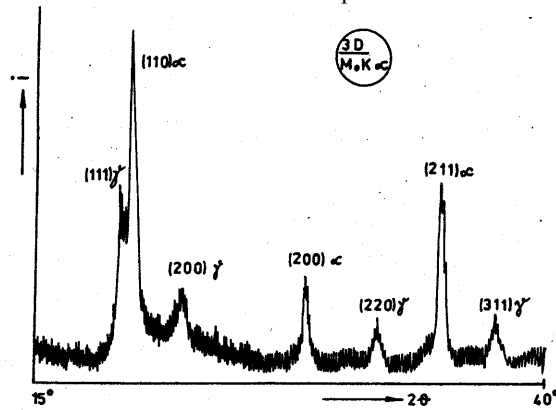


Fig. 2. Diffraction diagram of steel 40Cr10 nitrated and tempered in electrolytic plasma – sample 3D

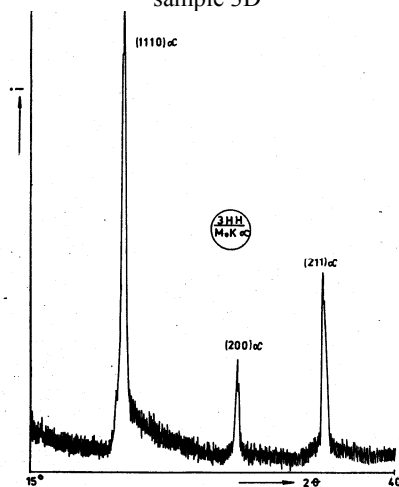


Fig. 3. Diffraction diagram of steel 40Cr10 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 3HH

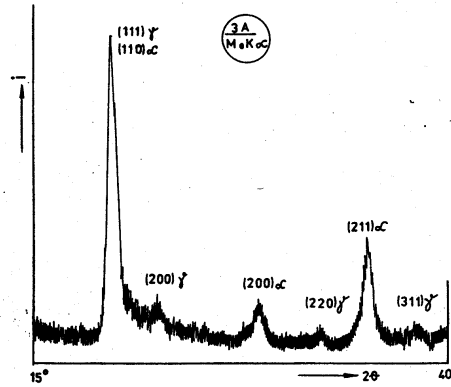


Fig. 4. Diffraction diagram of steel 40Cr10 nitrated and tempered in electrolytic plasma –sample 3A

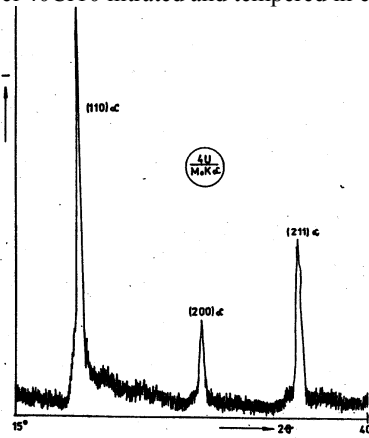


Fig. 5. Diffraction diagram of steel OLC 55 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 4V

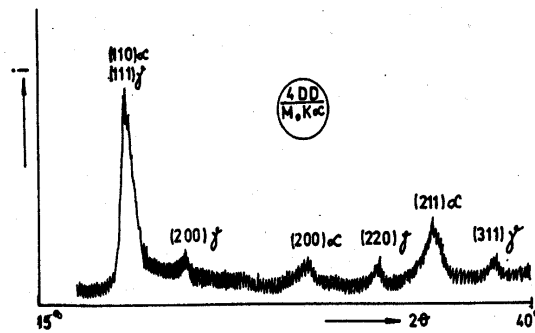


Fig. 6. Diffraction diagram of steel OLC 55 nitrated and tempered in electrolytic plasma –sample 4DD

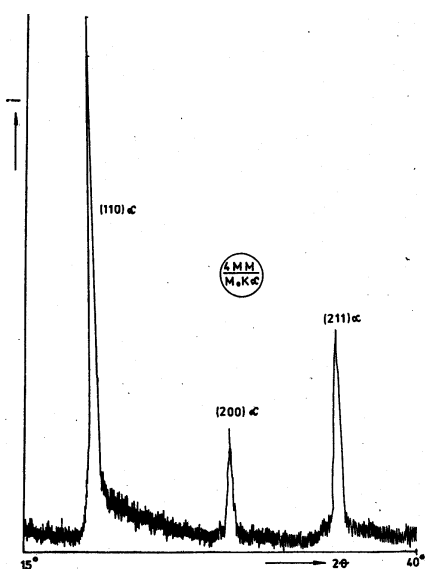


Fig. 7. Diffraction diagram of steel OLC 55 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 4MM

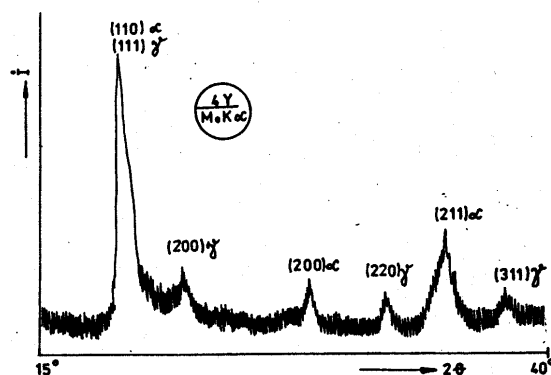


Fig. 8. Diffraction diagram of steel OLC 55 nitrated and tempered in electrolytic plasma – sample 4Y

Table 2

Plane spacing and phase nature presented in the structure of steel 40Cr10 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 3B

d_{hkl}	Phase	(h k l)
2,053	α	110
1,4378	α	200
1,1646	α	211

Table 3

Plane spacing and phase nature presented in the structure of steel 40Cr10 nitrated and tempered in electrolytic plasma – sample 3D

d_{hkl}	Phase	(h k l)
2,076	γ	111
2,024	α	110
1,8161	γ	200
1,4364	α	200
1,2857	γ	220
1,1763	α	211
1,0929	γ	311

Table 4

Plane spacing and phase nature presented in the structure of steel 40Cr10 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 3HH

d_{hkl}	Phase	(h k l)
2,024	α	110
1,4328	α	200
1,1692	α	211

Table 5

Plane spacing and phase nature presented in the structure of steel 40Cr10 nitrated and tempered in electrolytic plasma – sample 3A

d_{hkl}	Phase	(h k l)
2,076	$\alpha+\gamma$	$110_{\square}+111_{\square}$
2,024	α	110
1,8161	γ	200
1,4364	α	200
1,2857	γ	220
1,1763	α	211
1,0929	γ	311

Table 6

Plane spacing and phase nature presented in the structure of steel OLC 55 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 4V

d_{hkl}	Phase	(h k l)
2,0510	α	110
1,4369	α	200
1,1716	α	211

Table 7

Plane spacing and phase nature presented in the structure of steel OLC 55 nitrated and tempered in electrolytic plasma – sample 4DD

d_{hkl}	Phase	(h k l)
2,0680	$\alpha+\gamma$	$110_{\square}+111_{\square}$
1,8161	α	200
1,4364	α	200
1,2800	γ	220
1,1777	α	211
1,0908	γ	311

Table 8

Plane spacing and phase nature presented in the structure of steel OLC 55 nitrated and tempered in electrolytic plasma and subsequently blued at 350°C in oven – sample 4MM

d_{hkl}	Phase	(h k l)
2,0580	α	110
1,4443	α	200
1,1739	α	211

Table 9

Plane spacing and phase nature presented in the structure of steel OLC 55 nitrated and tempered in electrolytic plasma – sample 4Y

d_{hkl}	Phase	(h k l)
2,0686	$\alpha+\gamma$	$110_{\alpha}+111_{\gamma}$
1,8278	α	200
1,4400	α	200
1,2800	γ	220
1,1787	α	211
1,0904	γ	311

As for the concentration of the phases present in the structure of the samples investigated, we determined the values presented below table 10.

Table 10

Technological parameters for thermal and thermal-chemical treatment in electrolytic plasma

Sample	v_{α} , [%]	v_{γ} , [%]	v_N , [%]
3B	100	-	-
3D	78,30	21,70	-
3HH	100	-	-
3A	65,80	8,30	25,90
4V	100	-	-
4DD	70,30	12,40	17,40
4MM	100	-	-
4Y	64,70	14,10	21,20

4. Conclusions

1. The Roentgen structural investigations effectuated pointed out the nature of phases present in the structure of the two steels processed thermally in electrolytic plasma: nitrogen-based martensite (nitromartensite); residual austenite and chemical compounds (nitrites).

2. The structural phases identified correspond to the thermal-chemical treatment applied, their concentration being dependent on the two main technological parameters: temperature and diffusion time.

3. Thus, in the improving steels 40Cr10 and OLC 55 nitrated, we notice a reduction of the nitride quantity once with the increase of the diffusion temperature.

4. The application of bluing in oven after nitration and tempering in electrolytic plasma has as effect the complete transformation of the residual austenite in cubic martensite.

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Baci Maria – Doctor of Engineering Sciences, Associate Professor, Faculty of Science and Engineering Materials, tel.: 0232-278688, e-mail: maria baci_2004@yahoo.com

Rusu Ion - Doctor of Engineering Sciences, Associate Professor, Faculty of Science and Engineering Materials, tel.: 0232-278688, e-mail: vrusu 2003@yahoo.com
Technical University “Gheorghe Asachi” from Iasi, Romania.